

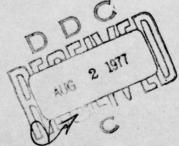
DCIEM Technical Report No. 77X6



A NOISE SURVEY OF THE CORMORANT, PROPOSED FDSS

R.B. Crabtree

DISTRIBUTION STATEMENT A
Approved for public release;
Distribution Unlimited



DEFENCE AND CIVIL INSTITUTE OF ENVIRONMENTAL MEDICINE INSTITUT MILITAIRE ET CIVIL DE MEDECINE DE L'ENVIRONNEMENT

DEPARTMENT OF NATIONAL DEFENCE - CANADA

SEPTEM 1976

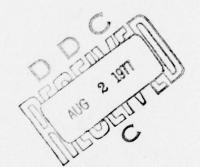
DCIEM Technical Report No. 77X6

12 42 p.)

DDCIEM-77-17-X-6

6

A NOISE SURVEY OF THE CORMORANT, PROPOSED FDSS



R.B. Crabtree



Behavioural Sciences Division
Defence and Civil Institute of Environmental Medicine
1.133 Sheppard Avenue West, P.O. Box 2000
Downsview, Ontario M3M 3B9

DEPARTMENT OF NATIONAL DEFENCE - CANADA

406986

Ince

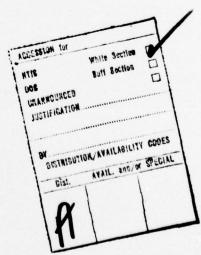
TABLE OF CONTENTS

	Page
ABSTRACT	v
INTRODUCTION	1
PROCEDURE	1
NOISE PROFILE	2
HABITABILITY	3
DAMAGE RISK TO HEARING	4
HEARING CONSERVATION	6
OPERATIONS	6
CONCLUSIONS	7
ACKNOWLEDGMENT	10
REFERENCES	11
FIGURES	12
APPENDICES	
A Noise levels in the main machinery spaces of the CORMORANT running at high speed (11 knots)	28
B Noise levels in selected locations at cruise speed (8 knots)	29
C Noise levels in selected areas at low speed (4 knots)	30
D Noise levels in selected areas at dockside	31
E Other noise levels	32
F Steady-state noise exposure limits	34
G Speaker-listener distances for face-to-face voice communication as limited by ambient noise	35
H DND specification for airborn noise in shipboard spaces	36

ABSTRACT

A noise survey was conducted on board the CORMORANT, proposed FDSS (Formerly the ASPA QUARTO), in her original trawler configuration to determine if noise would be a habitability, health or operational problem after the FDSS refit.

It was found that in sleeping quarters adjoining the main machinery spaces, noise will probably cause sleep and rest disturbance unless adequate noise reduction measures are implemented, and that a hearing hazard exists for persons occupying the main machinery spaces on a routine basis. In addition, the proposed communications/control complex will require considerable quieting of the Diesel Generator Room exhaust blowers.



- v -

INTRODUCTION

In response to tasking from NDHQ, the Human Engineering Section of DCIEM conducted an ergonomics investigation of the CORMORANT¹ (formerly the ASPA QUARTO) (Figure 1), an Italian stern trawler, as a prerequisite to her refit as a CF Fleet Diving Support Ship (FDSS). As part of this evaluation, the Sonics Section performed a study of the noise environment of the ship in her original configuration to determine if noise, as it existed, would be a habitability, health, or operational problem after the refit. This report presents the results of the noise survey and makes appropriate recommendations.

PROCEDURE

The noise evaluation was conducted in February 1976 during trials at the Underwater Range off Halifax and at the Halifax Dock Yards. Overall and octave-band sound pressure levels were measured using a Bruel and Kjaer, type 2209, precision sound level meter and a type 1613 octave filter set. In addition, the noise in certain compartments was recorded with a Nagra, type IV-S, precision tape recorder. Results of the noise analysis are tabulated in Appendices A to E.

ASPA QUARTO, a 240-foot fishing trawler purchased by DND is to be refitted into a mother ship for the Submersible Diver Lockout (SDL) research submarine, and a base for related diving activities. She is powered by three 900 hp turbocharged diesel engines, each driving a 730 kva alternator. These units can be switch-connected to either the propulsion buss or the service buss as required. The variable-pitch propeller is driven at 200 rpm (nominally) by two 950 hp electric motors operating into a common gearbox.



NOISE PROFILE

The distribution of A-weighted² sound pressure levels throughout the ship is shown in profile in Figure 2. Plan views of Nos. 01, 1 and 2 Decks (Figures 3, 4 and 5 respectively) illustrate this distribution in greater detail in the vicinity of the Diesel Generator Room casing. The main machinery spaces (the Diesel Generator Room and Propulsion Machinery Room) contain the most intense noise found on the ship. Noise in the areas adjacent to the Diesel Generator Room, although not intense enough to be a serious hazard to hearing, interfere with conversation and may disturb sleep.

The type of propulsion system³ used on the ship is such that the noise from the diesel generators changes minimally with ship speed/engine loading. The octave-band noise levels observed at the Switchboard (in the Diesel Generator Room) increase only slightly, for example, from zero ship speed with engines idling to 11 knots at nearly full power (Figure 6).

A sound having energy which is concentrated in the 20- to 500-Hz range produces a sensation that is less loud than a sound with an equal amount of energy in the frequency range 500 to 5000 Hz. In addition, a high-intensity low-frequency sound causes less hearing damage than a sound with an equivalent amount of mid-frequency energy. Thus, when an estimate of the loudness or hearing-damage potential of continuous noise is required, its low-frequency components are de-emphasized. One particular frequency weighting, the A-weighting, applies approximately 30 dB of de-emphasis at 50 Hz, and decreases to 5 dB at 500 Hz and 0 dB at 1000 Hz. The C-weighting, on the other hand, applies virtually no de-emphasis in the audible-frequency range. The sound pressure level of a sound, expressed in dB, is assumed to be C-weight unless otherwise specified. Sound pressure levels that are A-weighted are expressed as dBA.

³ The diesel generators and propulsion motors on this ship run at nominal speeds of 600 and 1800 rpm respectively, with propulsion thrust being controlled solely by propeller pitch angle.

HABITABILITY

The high levels of noise existing in the Diesel Generator Room will present a problem in the areas directly adjacent to it. The C2 and P2 Quarters on Nos. 2 and 3 Decks respectively, designated as sleeping accommodation, will contain noise likely to cause sleep and rest disturbance.

The noise levels measured on both sides of the bulkhead immediately aft of the diesel generators are illustrated in Figure 7. Also shown is the PNC-60 Preferred Noise Criterion Curve (Beranek et al, 1971), which describes the maximum recommended octave-band noise levels (65 dBA) for shipboard sleeping quarters⁴. It can be seen that considerable noise reduction is required, particularly in the low frequency octave-bands, in order to meet this specification.

Since the low frequency attenuation of the bulkhead (3 to 5 dB) is less than might be expected from this type of barrier, it appears that acoustic energy is being transmitted around it by the structural members of the ship, to which the diesel generators are rigidly mounted. Resilient supports would substantially reduce structureborn noise from this source.

In areas where a lobby or companionway will separate the Diesel Generator Room from sleeping quarters (e.g., the officers' accommodation on No. 1 Deck), additional noise reduction would result from the double barrier (Appendix E). However, where sleeping accommodation is located over a part of the machinery room, the section of decking separating the two areas will undoubtedly require acoustic treatment.

It is interesting to note that the refrigeration insulation in No. 1 Hold (Figure 8), consisting of a thick wall of foam sandwiched between steel plating and concrete, provides a better noise barrier (subjectively, the noise is far less obtrusive) than does the plating, air-space, composition-board construction found in the corridor on No. 2 Deck and in most other areas (Figure 7).

Noise Criteria for Sleeping Quarters Onboard Canadian Forces Ships (Forshaw, 1975).

DAMAGE RISK TO HEARING

The noise produced by the main engines is sufficiently intense to be a definite risk to the hearing of crew members without hearing protection who must occupy the Diesel Generator Room on a routine basis.

For hearing conservation purposes, CFAO 34-22 specifies noise exposure limits in terms of ISO Noise Rating Numbers 5 (Forshaw, 1970). Maximum continuous exposure times vary from eight hours per day for noise having a Noise Rating Number not greater than N-85 to only four minutes per day for noise of N=125 (Appendix F). Noise exposures within these limits are considered to be non-hazardous in the long term for most people.

Accordingly, the noise hazard to hearing for Diesel Generator Room personnel is summarized in Table 1, for cruise-speed and zero-speed conditions. The Switchboard and No. 1 Diesel Generator are illustrated in Figures 10 and 11 respectively.

The levels of noise in the Propulsion Machinery Room are such that unprotected exposure should be limited to 22 or 45 minutes per day. However, this space is occupied only during outer round duties and maintenance operations (Appendices A to E and Figure 12).

The octave-band spectra of the noise at the locations listed in Table 1 are shown in Figure 9. With the exception of the Engineers' Workshop and areas very close to the engines (within the near sound field), the noise levels throughout the Diesel Generator Room are similar in both intensity and spectrum.

The International Organization for Standardization (ISO) Noise Rating Curves are an agreed set of empirical curves relating octave-band sound pressure levels to the centre frequency of the octave-bands. Each curve is characterized by a Noise Rating Number (N), which is numerically equal to the sound pressure level of the curve at 1000 Hz. The Noise Rating of a given noise can be found by plotting the octave-band spectrum on the Noise Rating Curves and selecting the highest curve to which the spectrum is tangent.

TABLE 1

MAXIMUM DAILY NOISE EXP	OSURE LIMITS FOR DIESE	
	MAXIMUM DAILY EXPOSUR	E TIME IN MINUTES
LOCATION	8 KNOTS	ZERO KNOTS (engines idling)
Switchboard (principal watchkeeping station)	45*	45
No. 4 deck aft, between Diesel Generators Nos. 2 and 3	22	22
Access platform, No. 2 deck level	45	120
Access platform, No. 1 deck level	120	120
Engineers' Workshop	No data	480

 $[\]star$ Noise exposure at the Switchboard is reduced to 22 minutes at high speed.

When noise exposures are interrupted by sufficiently long recovery periods in which the ambient noise does not exceed ISO Noise Rating Number N=85, or 90 dBA, considerably longer cumulative exposures may be tolerated by the ear (Forshaw, 1970).

HEARING CONSERVATION

The unprotected noise exposure limits specified above for machinery space personnel are impractical, given that normal watchkeeping routines are of three- or four-hour durations. For prolonged exposures, therefore, hearing protection must be worn throughout these areas if the risk of significant hearing loss is to be minimized. The estimated levels of noise under the CF standard issue earmuffs (SSC 258), worn by a person stationed at the Switchboard, are illustrated in Figure 13 (Clark et al, 1967). Clearly, hearing protection reduces the noise at the ears to levels which are non-hazardous in the long term. All machinery space personnel should therefore be provided with effective hearing protectors on a personal issue basis.

OPERATIONS

In order to determine if noise might affect the efficiency of the ship's operations, measurements were made on No. 1 Deck in areas proposed for the FDSS Communications/Control complex (Figure 3). Levels of noise ranged from 85 dBA in the proposed Red Area (presently the XO's washroom), to 61 dBA on the Bridge (Figures 14 and 15). The principal sources of noise in this area are the main machinery-space exhaust blowers which generate spectra characterized by a large pure tone component in the 250-Hz octave-band. This can be seen (Figure 16) in the noise observed on the Bridge, in the Lobby, and particularly in the washroom (proposed Red Area).

Obviously, the noise measured in these areas will be affected by the planned structural changes. Although it is difficult to predict exactly what the resultant noise levels will be after refit, some generalizations can be made:

- 1. The sound absorptive layer proposed for the walls of the Red Area should insure that noise inside the room is below levels considered hazardous to hearing. However, the whine-like character of the noise will undoubtedly annoy the man stationed there. Noise treatment of the blower compartment, or the blowers themselves (perhaps by Helmholtz absorptive resonators), would further reduce this noise.
- 2. The curtain which is planned to separate the Red Area and Communications Area will be acoustically transparent to low frequency noise and will therefore be ineffective in preventing blower noise from entering the Communications

Area. It is noted that the maximum allowable noise level for manned radio rooms is 63 dBA, as specified in the DND Noise Criteria for Shipboard Spaces (CDA/MS/NVSH 1-0-1, Anon, 1972). Unless an effective noise attenuating partition is installed between these areas, it will be impossible to meet this criterion.

An additional noise barrier, constructed along the Diesel Generator Room casing, would attenuate the midand high-frequency noise transmitted through the casing.

- 3. Levels of noise will be lower in the Underwater Tracking Area than in the Communications Area due to the barrier partition between them. It is unlikely that the former will be as quiet as the Bridge in its original configuration or that it will meet the NVSH specification of 58 dBA for sonar control rooms.
- 4. The noise levels on the Bridge did meet the NVSH requirement. There is no reason to believe that this will change after the refit.

Observations made on the Bridge suggest that the telephone system used on the ship is not adequate for communicating in areas containing high ambient levels of noise (e.g., the Diesel Generator and Propulsion Machinery Rooms) due to distortion of the speech signals and masking by the noise. Noise-excluding hoods should be installed at telephone locations in high noise areas to improve speech intelligibility.

CONCLUSIONS

General

- The most intense levels of noise found on the CORMORANT exist in the Diesel Generator Room and in the Propulsion Machinery Room.
- 2. Noise levels in the Diesel Generator Room do not vary appreciably with ship speed.

Habitability

CONTRACTOR DE SECURITARIO DE SECURITARIO.

 Areas that adjoin the main machinery spaces, and/or are directly over a part of the main machinery spaces, contain high levels of noise and will be unacceptable as sleeping quarters.

- 2. Sizable noise reductions in noise-critical areas can be achieved by:
 - a) the construction of effective noise barriers, particularly at the Diesel Generator Room casing,
 - b) separation of the sleeping quarters from the Diesel Generator Room by means of a corridor or lobby, thereby forming a double noise barrier, and
 - c) resilient mounting of the diesel generator units to reduce the transmission of structure-born noise from the engines.

Damage Risk to Hearing and Ear Protection

Noise produced by the main engines or propulsion motors and gearing is sufficiently intense under most operating conditions to be hazardous to the hearing of crew members who routinely occupy the main machinery spaces for more than 22 to 45 minutes per day. Since watchkeeping routines in these areas are usually of three to four hours duration, effective ear protection must be worn by these people if the risk of significant hearing loss is to be minimized. All machinery space personnel should be provided with their own CF standard issue ear muffs.

Operations

- 1. The noise levels at locations that will form part of the FDSS operations/communications area are presently as much as 22 dBA in excess of recommended levels (CDA/MS/NVSH 1-0-1). The main source of this noise is the exhaust blowers for the Diesel Generator Room, located adjacent to the proposed Red Area. It is clear that substantial quieting of these blowers is necessary.
- 2. Noise levels on the existing bridge meet the NVSH specification.

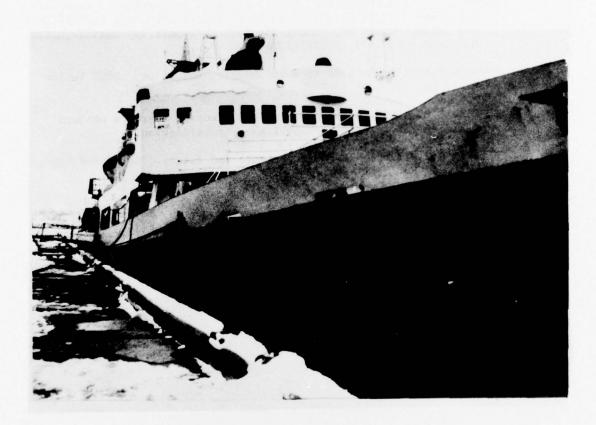
3. The telephone system on the ship may not provide adequate communication in areas where the ambient level of noise is very high. The use of noise-excluding hoods around the telephones is recommended for such compartments.

ACKNOWLEDGEMENT

The author wishes to thank the acting Commanding Officer of the CORMORANT, LCDR Dale Gibb, for the excellent support and co-operation provided by the ship's officers and men during this investigation.

REFERENCES

- ANON. (1972) Specification for airborne noise criteria for shipboard spaces. Department of National Defence CDA/MS/NVSH 1-0-1, Issue 3.
- BERANEK L.L., WARREN E.B. & FIGWER J.J. (1971) Preferred noise criterion (PNCP curves and their application to rooms. Jour Acoust Soc Am., 50, pp 1223-1228.
- CLARK D.P.J. & LEDERMAN S.J. (1967) Acoustic properties of headgear: XXV. David Clark Co. "Straightaway" Models E800, 10A and C6502G01 and Safety Supply Co. Model 258 Safe-T-Earmuff (U) DRET Technical Memorandum No. 677 (RESTRICTED).
- FORSHAW S.E. (1970) Guide to noise-hazard evaluation. DRET Review Paper No. 771.
- FORSHAW S.E. (1975) Noise criteria for sleeping quarters onboard Canadian Forces ships. Unpublished Specification.
- WEBSTER J.C. (1969) SIL-Past, present, and future. Sound and Vibration, 5, No. 8, 22-26.



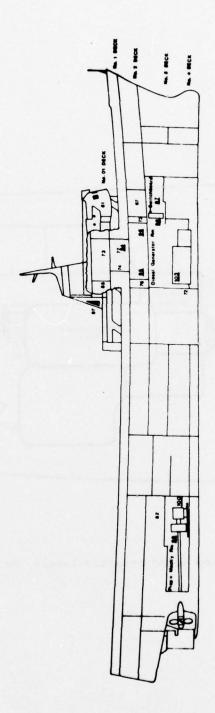


Figure 2: Noise profile of the CORMORANT in A-weighted sound pressure levels. Underlined numbers indicate measurements taken within the main machinery spaces.

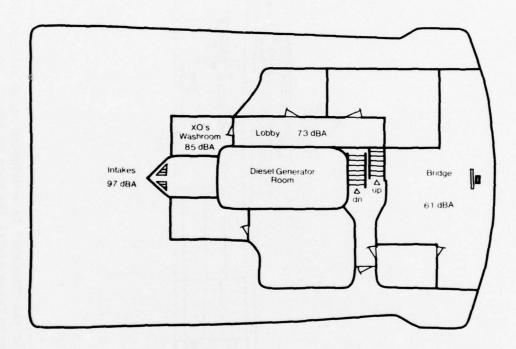


Figure 3: A-weighted sound pressure levels, No. 01 Deck.

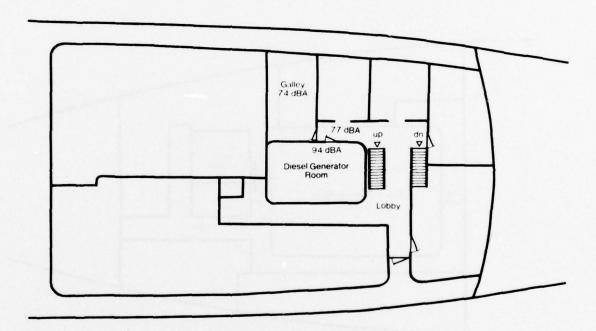


Figure 4: A-weighted sound pressure levels, No. 1 Deck.

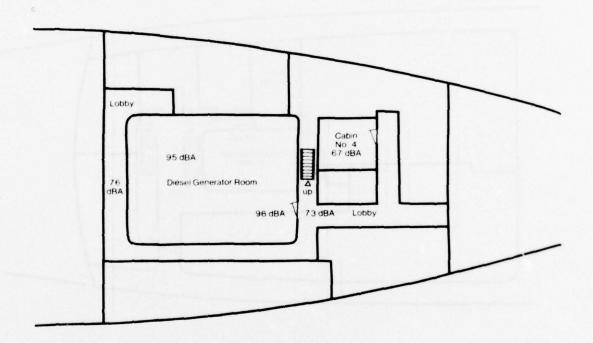


Figure 5: A-weighted sound pressure levels, No. 2 Deck.

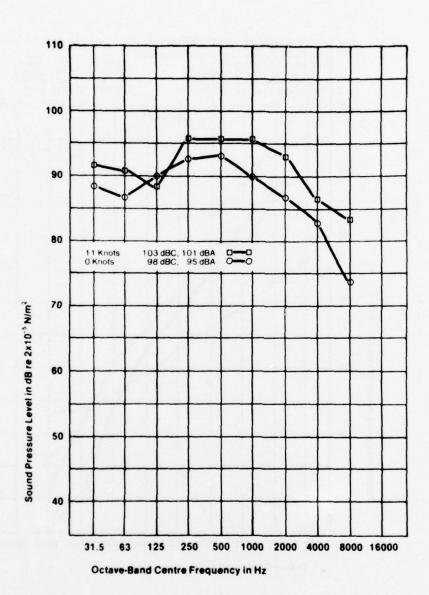


Figure 6: Overall and octave-band sound pressure levels at the Switchboard 1) at 11 knots, 90% propeller pitch (all diesel generators running), and 2) at dockside (diesel generators Nos. 1 and 2 running with no load).

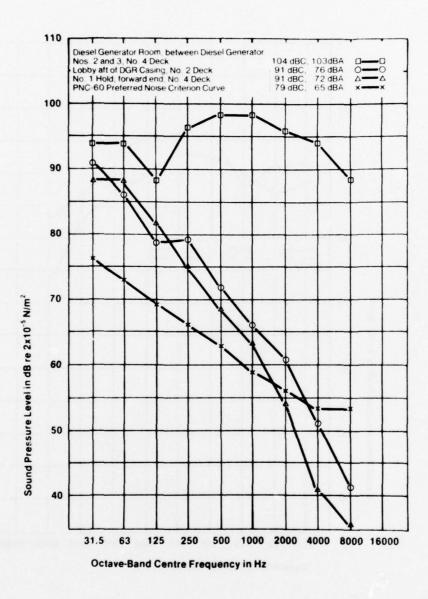
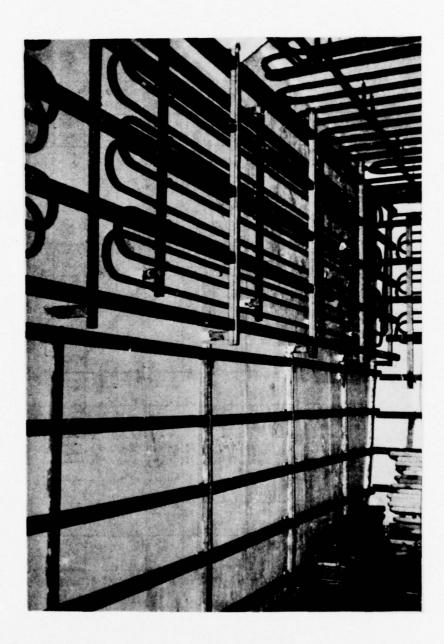
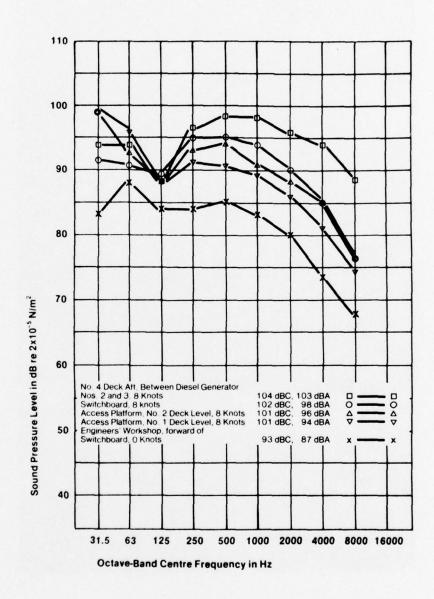


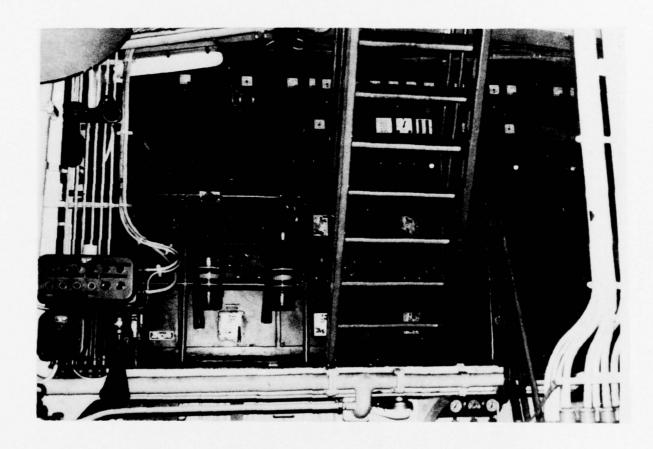
Figure 7: Overall and octave-band sound pressure levels at both sides of the bulkhead immediately aft of the diesel generators, and Preferred Noise Criterion Curve PNC-60.



 $\frac{\textbf{Figure 8:}}{\textbf{Generator Room casing in No. 1 Hold.}}$



 $\frac{\text{Figure 9:}}{\text{locations in the Diesel Generator Room with all three diesel generators}}$



 $\underline{\mbox{Figure 10:}}$ The main Switchboard viewed from beside No. 2 Diesel Generator.

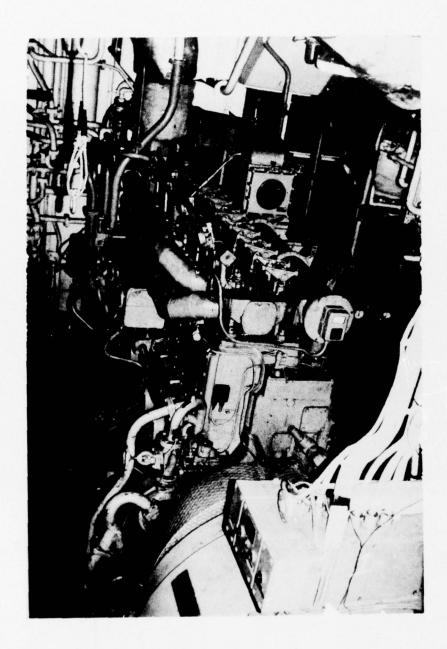


Figure 11: No. 1 Diesel Generator viewed from the Switchboard.

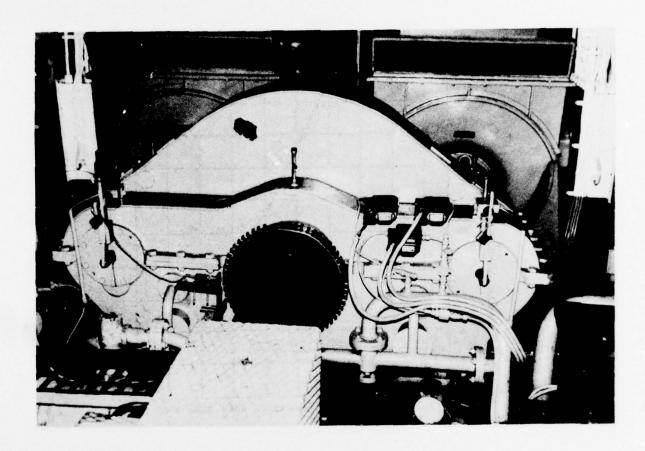


Figure 12: The propulsion motors and main gearing.

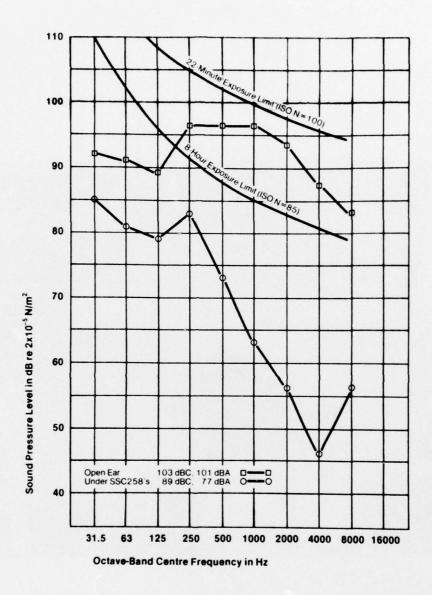


Figure 13: Overall and octave-band sound pressure levels at the Switchboard at 11 knots showing 1) actual levels, and 2) those expected under a set of SSC 258 standard issue earmuffs. (The earmuff attenuation shown in each octave band is the mean attenuation less one standard deviation). Also shown are ISO Noise Rating Curve Nos. 100 and 85.

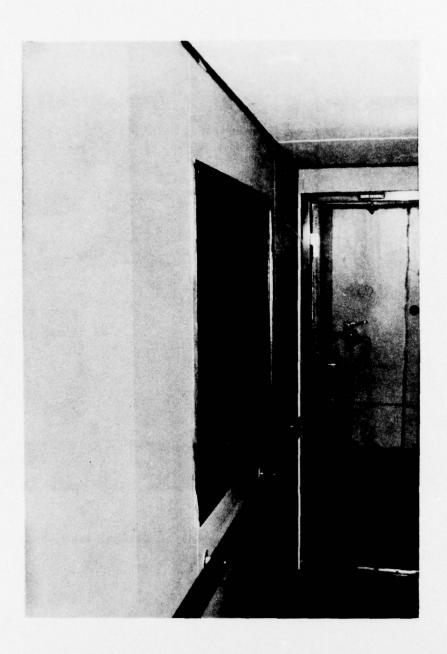


Figure 14: The Lobby, port side of the Diesel Generator Room Casing, No. Ol Deck looking towards the Executive Officer's Washroom.



Figure 15: A view of the command position on the Bridge, from the starboard side.

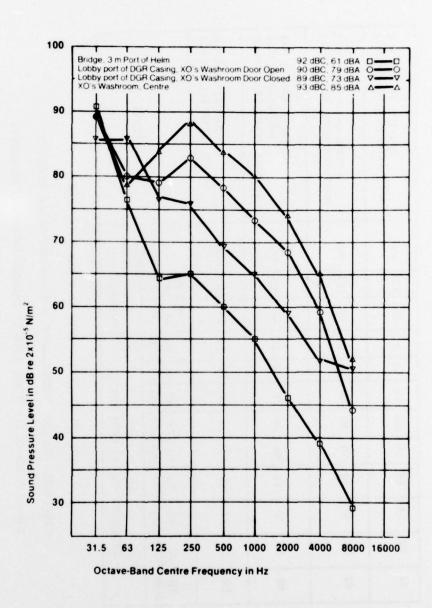


Figure 16: Overall and octave-band sound pressure levels at three locations on No. 01 Deck.

APPENDIX A

OVERALL AND OCTAVE-BAND SOUND PRESSURE LEVELS IN THE MAIN MACHINERY

SPACES OF CORMORANT RUNNING AT HIGH SPEED (11 KNOTS WITH 90% PROPELLER PITCH AND 200 RPM SHAFT SPEED. DIESEL GENERATORS

NOS.
;
2
AND
w
NO NO
PROPULSION/
SERVICE
BUSS)

1 OCATION	ISO OVERALL NOISE SPL	OVERA SPL	PL		20	AVE	BANI	AND CENTRE SPLS IN dB	dB I	OCTAVE BAND CENTRE FREQUENCY SPLS IN dB	NCY	
POCALTON	NO.	C Wt dBC	A Wt dBA	31.5 Hz	63 Hz	125 Hz	63 125 250 Hz Hz Hz	500 Hz	500 1000 Hz Hz	31.5 63 125 250 500 1000 2000 4000 8000 Hz Hz Hz Hz Hz Hz Hz Hz Hz	4000 Hz	zH 0008
Diesel Generator Room at Switchboard	100	103	103 101	92	91	89	96	96	96	93	87	83
Diesel Generator Room at Access Platform No. 2 Deck Level	95	102	102 100	97	91	87	87 95 94	94	95	91	87	84
Propulsion Machinery Room 1 m forward of Motors	100	104	104 103	97 92	92	92	90	94	98	96	85	79
Propulsion Machinery Room 1 m aft of Gearbox	100	104	104 102	94 91 91 90 97	91	91	90	97	98	95	84	76

APPENDIX B

OVERALL AND OCTAVE-BAND SOUND PRESSURE LEVELS IN SELECTED LOCATIONS OF CORMORANT RUNNING AT CRUISING SPEED (8 KNOTS WITH 70% PROPELLER PITCH. DIESEL GENERATORS NOS. 1 AND 2 ON PROPULSION BUSS, NO. 3 ON SERVICE BUSS)

LOCATION	ISO NOISE RATING		RALL		oc	TAVE		CEN Ls II		FREQUI	ENCY	
LOCATION	NO.	C Wt dBC	200000	31.5 Hz	63 Hz			500 Hz	1000 Hz	2000 Hz	4000 Hz	8000 Hz
Diesel Generator Room at Switchboard	95	102	98	92	91	89	95	95	94	90	85	77
Diesel Generator Room at Access Platform, No. 2 Deck level	95	101	96	99	93	88	93	94	91	88	85	77
Diesel Generator Room at Access Platform, No. 1 Deck Ievel	90	101	94	99	96	87	92	91	89	86	82	74
Propulsion Machinery Room, 1 m forward of Motors	100	102	100	92	90	88	90	92	96	94	82	77
Propulsion Machinery Room, 1 m aft of Gearbox	95	102	99	92	94	91	90	91	95	92	82	72
Lobby aft of DGR Casing, No. 2 Deck		91	76	91	86	78	79	72	66	60	52	42
Lobby outside DGR Access Door, No. 1 Deck		88	77	83	86	79	76	75	71	68	56	50
Lobby port of DGR Casing, No. 01 Deck, 2 m aft of Stairway		89	73	86	86	77	76	69	65	59	52	51
No. 1 Hold, 1 m aft of Forward Bulkhead,		91	72	88	88	82	75	68	63	54	41	36

APPENDIX C

OVERALL AND OCTAVE-BAND SOUND PRESSURE LEVELS IN SELECTED LOCATIONS OF CORMORANT
RUNNING AT LOW SPEED (4 KNOTS WITH 85% PROPELLER PITCH AND SHAFT SPEED
REDUCED TO 120 RPM, DIESEL GENERATORS NO. 1 ON PROPULSION BUSS (SPEED
REDUCED TO 350 RPM), 2 AND 3 ON SERVICE BUSS, NORMAL SPEED (600 RPM))

LOCATION	ISO NOISE RATING		RALL		oc	TAVE		CEI Ls II		FREQUI	ENCY	
LOCATION	NO. N	C Wt dBC		31.5 Hz	63 Hz	1		500 Hz	1000 Hz	2000 Hz	4000 Hz	8000 Hz
Diesel Generator Room at Swtichboard	90	98	95	88	89	87	92	92	90	86	78	70
Diesel Generator Room at Access Platform No. 2 Deck level	90	100	94	95	97	97	93	90	89	86	81	70
Diesel Generator Room at Access Platform, No. 1 Deck level	90	100	93	96	94	89	91	88	87	84	79	69
Propulsion Machinery Room, 1 m forward of Motors	95	96	94	77	80	83	87	91	91	86	79	70
Propulsion Machinery Room, 1 m aft of Gearbox	95	96	95	83	80	84	86	89	92	88	80	72
Lobby aft of DGR Casing, No. 2 Deck		91	73	89	88	81	77	69	63	58	49	39
Lobby outside DGR Access Door, No. 1 Deck		87	75	82	84	80	79	74	70	66	59	45
Lobby port of DGR Casing, No. 01 Deck, 2 m aft of Stairway		92	74	89	82	78	77	70	66	60	51	41
No. 1 Hold, 1 m aft of forward Bulkhead, No. 4 Deck level		90	70	88	86	80	72	66	60	51	40	35

APPENDIX D

OVERALL AND OCTAVE-BAND SOUND PRESSURE LEVELS IN SELECTED LOCATIONS OF CORMORANT AT DOCKSIDE (PROPELLER FEATHERED, 200 RPM SHAFT SPEED.

DIESEL GENERATORS NOS. 2 AND 3 RUNNING)

LOCATION	ISO NOISE RATING	ACCURATION.	RALL		oc	TAVE		CE Ls I	NTRE I	FREQU	ENCY	
LOCATION	NO.	C Wt dBC	A Wt dBA	31.5 Hz	63 Hz		250 Hz		1000 Hz	2000 Hz	4000 Hz	8000 Hz
Diesel Generator Room at Switchboard	95	98	95	88	87	90	93	93	90	87	83	74
Diesel Generator Room at Access Platform, No. 2 Deck level	90	99	94	96	88	87	92	92	89	87	83	74
Diesel Generator Room at Access Platform, No. Deck level	90	98	92	96	90	86	90	90	86	85	81	71
Propulsion Machinery Room, 1 m forward at Motors	95	100	97	88	92	91	91	92	93	89	86	78
Propulsion Machinery Room, 1 m aft of Gearbox	100	103	100	93	96	97	95	94	96	91	95	78
Lobby aft of DGR Casing, No. 2 Deck		89	73	88	86	78	77	70	65	62	52	40
Lobby outside DGR Access Door, No. 1 Deck		82	75	76	76	76	77	73	69	66	61	49
Lobby port of DGR Casing, No. 01 Deck, 2 m aft of Stairway*		90	79	90	80	79	83	78	73	68	59	44
No. 1 Hold, 1 m aft of forward Bulkhead, No. 4 Deck level		87	68	84	84	76	72	67	60	52	38	25

^{*} The door of the XO's washroom was open during this measurement

APPENDIX E

OTHER OVERALL AND OCTAVE-BAND SOUND PRESSURE LEVELS RECORDED IN CORMORANT

		1SO NOISE	OVERALL SPL	ATT		007	AVE	SPI	AND CENTRE SPLS IN dB	dB	OCTAVE BAND CENTRE FREQUENCY SPLs IN dB	ENCY	
LOCALION	CONDITIONS	NO.	dBC C	C A WE WE	31.5 63 125 Hz Hz Hz	63 Hz	125 Hz	250 Hz	500 Hz	500 1000 Hz Hz	2000 Hz	2000 4000 8000 Hz Hz Hz	2H 2008
Diesel Generator Room, between Diesel Genera- tors Nos. 1 and 2, on Catwalk, No. 2 Deck	0 Knots, Diesel Generators Nos. 2 and 3 Running	95	99	95	86	90	89	93	92	91	80	. %	75
Diesel Generator Room, between Diesel Genera- tors Nos. 2 and 3 No. 4 Deck level, 1 m from aft bulkhead	O Knots, Diesel Generators Nos. 1 and 3 Running	100	102	102 100	90	90	88	95	96	94	93	92	85
	8 Knots, Diesel Generators Nos. 1, 2 & 3 Running	100	104	103	104 103 94	94	88	97	98	98	96	94	88
Diesel Generator Room, Engineers' Workshop Centre	O Knots, Diesel Generators Nos. 1, 2 & 3 Running	85	93	87	83	87	84	84	85	83	80	73	67
Propulsion Machinery Room, 1 m forward of Motors	4 Knots, 70% Pitch 150 RPM Shaft	98	95	93	80	82	82	86	90	8	86	78	70
Propulsion Machinery Room, 1 m aft of Gearbox	4 Knots, 70% Pitch 150 RPM Shaft	90	96	95	84	83	83	85	88	93	87	8	22
Outside, No. 01 Deck 1 m aft of Diesel Generator Room, Air Intakes	4 Knots, Diesel Generators Nos. 1, 2 & 3 Running 85% Pitch, 120 RPM Shaft	95	101	97	95	88	86	98	94	92	8	8	73

APPENDIX E (CONTINUED)

	0 2	0			2	m	1 ~1
	800 Hz	29	17		4.2	63	52
ENCY	31.5 63 125 250 500 1000 2000 4000 8000 Hz Hz	39	55	77	55	73	65
OCTAVE BAND CENTRE FREQUENCY SPLS IN dB	2000 Hz	47	59	96	63	78	74
ND CENTRE I	1000 Hz	55	70	63	99	82	80
CEN Ls]	500 Hz	09	72	89	70	83	84
BAND	250 Hz	65	75	70	73	82	88
AVE	125 Hz	79	72	73	75	80	78
00	63 Hz	77	73	92	82	87	78
	31.5 Hz	91	78	73	88	93	06
ALL	A Wt dba	61	74	67	73	85	85
OVERALL SPL	C Wt dBC	92	82	97	88	76	93
SNOTTIMOS		O Knots, Diesel Generators Nos. 2 & 3 Running	O Knots, Diesel Generators Nos. 1 & 3 Running	O Knots, Diesel Generators Nos. 1, 2 & 3 Running	O Knots, Diesel Generators Nos. 1 & 3 Running, Access Door closed	Access Door Open	O Knots, Diesel Generators Nos. 1, 2 & 3 Running
NOTTAGE	NOT USO	Bridge, 3 m port of Helm	Galley Centre	Cabin No. 4, Centre	Lobby outside Diesel Generator Room Access Door,	No. 2 Deck	XO's Washroom Centre

APPENDIX F

STEADY-STATE NOISE EXPOSURE LIMITS

The maximum allowable time per day that an individual may be exposed to a continuous noise of given Noise Rating Number is presented below (CFAO 34-22).

ISO NOISE RATING NUMBER (N)	85	06	95	100	105	110	100 105 110 115 120	120	125
MAXIMUM ALLOWABLE EXPOSURE PER DAY IN MINUTES	480 120	120	45	22	14	11	8	9	7

APPENDIX G

VOICE LEVEL AND DISTANCE BETWEEN SPEAKER AND LISTENER FOR SATISFACTORY FACE-TO-FACE COMMUNICATION, AS LIMITED BY AMBIENT NOISE LEVEL (dBA)

(After Webster, 1969)

DISTANCE IN FEET BETWEEN SPEAKER AND LISTENER	NORMAL VOICE	EXPECTED VOICE LEVEL (1)	LIMIT FOR UN- AIDED FACE-TO- FACE SPEECH COMMUNICATION (2)
	A-WE	IGHTED AMBIENT S	OUND PRESSURE LEVEL
0.5	82 dBA	94 dBA	117 dBA
1	76 dBA	85 dBA	111 dBA
2	70 dBA	77 dBA	103 dBA
3	66 dBA	72 dBA	101 dBA
4	64 dBA	69 dBA	99 dBA
6	62 dBA	62 dBA	95 dBA
8	60 dBA	61 dBA	93 dBA
10	56 dBA	57 dBA	91. dBA
12	54 dBA	54 dBA	89 dBA

^{1.} The expected voice level is that to which normal-hearing persons would be expected to increase their vocal efforts to overcome masking effects of ambient noise upon their auditory feedback. This increase in vocal effort is about 3 dB for each 10 dB increase in ambient noise level, at a level starting at about 50 dB.

^{2.} Limited by maximum vocal effort.

APPENDIX H

DND SPECIFICATION FOR AIRBORNE NOISE CRITERIA

FOR SHIPBOARD SPACES1

(Anon, 1972)

	SHIP'S	SPEED		SHIP'S	SPEED
Operational Spaces	CRUISE ²	FULL ³		CRUISE ²	FULL ³
Command Position, Bridge	63 dBA	65 dBA	Operations Room	58 dBA	63 dBA
Sonar Control Room Target Indication Room	50 dBA 63 dBA	58 dBA 63 dBA		63 dBA 63 dBA	68 dBA 63 dBA
Radio (Manned)	58 dBA	63 dBA		77 dBA	77 dBA
Radio (Unmanned)	68 dBA	77 dBA	Gun Fire Control Room	63 dBA	63 dBA
Message Centre	68 dBA	68 dBA	Crypot Centre Gyro Room, Unmanned	68 dBA 77 dBA	68 dBA 91 dBA

Manned Working Spaces

Engine Room (general)	91	dBA	121	dBA	Boiler Room (general)	91	dBA	121	dBA
Engine Room (control console)	77	dBA	91	dBA	Boiler Room (control console)	77	dBA	91	dBA
Diesel room (general)	121	dBA	121	dBA	Switchboard	77	dBA	77	dBA
Diesel room (control console)	91	dBA	91	dBA	Magazines	77	dBA	77	dBA
Main Mach. Control Room	68	dBA	68	dBA	Electronic Workshop	68	dBA	68	dBA
Workshops	91	dBA	91	dBA	A/S Mortar handling rooms	77	dBA	77	dBA
Ordnance Spares Compt	91	dBA	91	dBA					
Torpedo House	77	dBA	77	dBA					
Galley	77	dBA	77	dBA					

Living Spaces

C.O.'s Cabin	63 dBA	63 dBA	Sick Bay (Consult)	58 dBA	63 dBA
Officers Cabins	68 dBA	68 dBA	Sick Bay (Hospital)	63 dBA	68 dBA
Offices	68 dBA	68 dBA			
Ward Room	63 dBA	68 dBA			
Ward Room ante room	63 dBA	68 dBA			
Crews Dining Hall	68 dBA	77 dBA			
P.O.'s Dining Hall	68 dBA	77 dBA			
Seamens Mess Spaces	68 dBA	73 dBA			

 $^{^{}m l}$ Criteria have been converted from Air Noise Control (ANC) levels in dB to A-weighted Sound Pressure Levels in dBA.

² Cruising speed: up to 15 knots.

Full Speed: 20 knots upwards.

Unclassified

Security Classification

	DOCUME (Security classification of title, body of abstract as	NT CONTROL DATA - Find indexing annotation must be		ne overall document is classified)			
1.	ORIGINATING ACTIVITY	/	2a. DOCUMENT SECURITY CLASSIFICATION Unclassified				
	DCIEM		26. GROUP Behavioural Science				
3.	A NOISE SURVEY OF THE CORMO	PRANT, PROPOSED FDS	S				
4	DESCRIPTIVE NOTES (Type of report and inclusive dates) Technical Report						
5.	AUTHOR(S) (Last name, first name, middle initial) Crabtree RB.						
6.	September 1976	7a. TOTAL NO. thirty-si		7b. NO. OF REFS SIX			
8a.	PROJECT OR GRANT NO.	9a. ORIGINATO	9a. ORIGINATOR'S DOCUMENT NUMBER(S) 77X6				
8b.	CONTRACT NO.		9b. OTHER DOCUMENT NO.(S) (Any other numbers that may be assigned this document)				
10.	DISTRIBUTION STATEMENT						
	Unlimited						
11.	SUPPLEMENTARY NOTES	12. SPONSORIN DCIEM	12. SPONSORING ACTIVITY DCIEM				
13.	ABSTRACT						

A noise survey was conducted on board the CORMORANT, proposed FDSS (Formerly the ASPA QUARTO), in her original trawler configuration to determine if noise would be a habitability, health or operational problem after the FDSS refit.

It was found that in sleeping quarters adjoining the main machinery spaces, noise will probably cause sleep and rest disturbance unless adequate noise reduction measures are implemented, and that a hearing hazard exists for persons occupying the main machinery spaces on a routine basis. In addition, the proposed communications/control complex will require considerable quieting of the Diesel Generator Room exhaust blowers.

KEY WORDS

Ship noise/habitability
Ship noise/operations
Ship noise/hearing
Ship engine room noise
Noise/Naval vessels
Hearing Conservation

INSTRUCTIONS

- OHIGINATING ACTIVITY. Enter the name and address of the organization issuing the document.
- 2a. DOCUMENT SECURITY CLASSIFICATION: Enter the overall security classification of the document including special warning terms wherever applicable.
- 2b. GROUP. Enter security reclassification group number. The three groups are defined in Appendix 'M' of the DRB Security Regulations.
- 3. DOCUMENT TITLE Enter the complete document title in all capital letters. Tables in all cases should be unclassified. If a sufficiently descriptive trile cannot be selected without classification, show little classification with the usual one capital letter abbreviation in parentheses immediately following the title.
- DESCRIPTIVE NOTES: Enter the category of document, e.g. technical report, technical note or technical letter. If appropriate, enter the type of document, e.g. interim, progress, summary, annual or final. Give the inclusive dates when a specific reporting period is covered.
- AUTHOR(S). Enter the name(s) of author(s) as shown on or or the document. Enter last name, first name, middle initial.
 If military, show rank. The name of the principal author is an absolute minimum requirement.
- DOCUMENT DATE: Enter the date (month, year) of Establishment approval for publication of the document.
- TOTAI. NUMBER OF PAGES: The total page count should follow normal pagination procedures, i.e., enter the number of pages containing information.
- NUMBER OF REFERENCES: Enter the total number of references cited in the document.
- 8a. PROJECT OR GRANT NUMBER: If appropriate, enter the applicable research and development project or grant number under which the document was written.
- 8b. CONTRACT NUMBER If appropriate, enter the applicable number under which the document was written.
- 9a. ORIGINATOR'S DOCUMENT NUMBER(S). Enter the official document number by which the document will be idensified and controlled by the originating activity. This number must be unique to this document.

- 9b. OTHER DOCUMENT NUMBER(S): If the document has been assigned any other document numbers (either by the originator or by the sponsor), also enter this number(s).
- DISTRIBUTION STATEMENT: Enter any limitations on further dissemination of the document, other than those imposed by security classification, using standard statements such as:
 - "Qualified requesters may obtain copies of this document from their defence documentation center."
 - (2) "Announcement and dissemination of this document is not authorized without prior approval from originating activity."
- SUPPLEMENTARY NOTES: Use for additional explanatory notes.
- SPONSORING ACTIVITY: Enter the name of the departmental project office or laboratory sponsoring the research and development. Include address.
- 13. ABSTRACT: Enter an abstract giving a brief and factual summary of the document, even though it may also appear elsewhere in the body of the document itself. It is highly desirable that the abstract of classified documents be unclassified. Each paragraph of the abstract shall end with an indication of the security classification of the information in the paragraph (unless the document itself is unclassified) represented as (TS), (S), (C), (R), or (U).

The length of the abstract should be limited to 20 single-spaced standard typewritten lines; 7½ inches long.

14. KEY WORDS: Key words are technically meaningful terms or short phrases that characterize a document and could be helpful in cataloging the document. Key words should be selected so that no security classification is required. Identifiers, such as equipment model designation, trade name, military project code name, geographic location, may be used as key words but will be followed by an indication of technical context.